AMENDMENTS TO THE CLAIMS:

List of Claims:

1. (Currently Amended) A fender formed from a rubber composition containing 20 to 80 parts by weight of carbon black and 0 to 20 parts by weight of softener based on 100 parts by weight of a base rubber selected from the group consisting of natural rubber, synthetic rubber and mixtures thereof, wherein said rubber composition has a rate of change of compressibility R_{-30}/R_{23} of not more than 1.3 (where R_{-30} denotes a maximum reaction force at -30°C as determined by compressive test and R_{23} denotes a maximum reaction force at 23°C as determined by compressive test) and/or a rate of change of compressibility R_{60}/R_{23} of more than 0.90 (where R_{23} denotes the maximum reaction force at 23°C and R_{60} denotes a maximum reaction force at 60°C).

2. (Previously Presented) The fender according to claim 1, wherein said rubber composition has the rate of change of compressibility R_{-30}/R_{23} of not more than 1.3 (where R_{-30} denotes the maximum reaction force at -30°C as determined by compressive test and R_{23} denotes the maximum reaction force at 23°C as determined by compressive test), thus imparting the fender with a sufficient compressive energy absorptivity for functioning as a shock absorber in a low-temperature range.

3. (Previously Presented) The fender according to claim 2, wherein said rubber composition has:

(i) a rate of change of rigidity modulus $G_{-30}/G_{23}<1.38$ and $\tan\delta<0.07$ as determined by dynamic shearing test (where G_{-30} and G_{23} denote dynamic moduli of rigidity at -30°C and at 23°C, respectively, as measured under the conditions of a frequency at 0.3Hz and a displacement of 2.5mm); and

(ii) a rate of change of elasticity modulus $E^*_{-30}/E^*_{23}<2.3$ and $\tan\delta<0.10$ as determined by dynamic tensile test (where E^*_{-30} and E^*_{23} denote dynamic moduli of elasticity in tension at -30°C and at 23°C, respectively, as measured under the conditions of a frequency at 10Hz and a displacement of 50μm).

4. (Previously Presented) The fender according to claim 1, wherein said rubber composition has the rate of change of compressibility R_{60}/R_{23} of more than 0.90 (where R_{23} denotes the maximum reaction force at 23°C and R_{60} denotes the maximum reaction force at 60°C), thus imparting the fender with a sufficient compressive energy absorptivity for functioning as a shock absorber in a high-temperature range.

5. (Previously Presented) The fender according to claim 4, wherein said rubber composition has:

(i) a rate of change of rigidity modulus $G_{60}/G_{23}>0.9$ and $\tan\delta<0.11$ as determined by dynamic shearing test (where G_{60} and G_{23} denote dynamic

moduli of rigidity at 60°C and at 23°C, respectively, as measured under the conditions of a frequency at 0.3Hz and a displacement of 2.5mm); and

(ii) a rate of change of elasticity modulus $E^*_{60}/E^*_{23}>0.7$ and $\tan\delta<0.14$ as determined by dynamic tensile test (where E^*_{60} and E^*_{23} denote dynamic moduli of elasticity in tension at 60°C and at 23°C, respectively, as measured under the conditions of a frequency at 10Hz and a displacement of 50μm).

Claim 6 (Cancelled)

7. (Previously Presented) A method for producing a fender from a rubber composition as a base material, wherein the rubber composition is prepared as an elastic base material and has a rate of change of compressibility R_{-30}/R_{23} of not more than 1.3 (where R_{-30} denotes a maximum reaction force at -30°C as determined by compressive test and R_{23} denotes a maximum reaction force at 23°C as determined by compressive test) and a rate of change of compressibility R_{60}/R_{23} of more than 0.90 (where R_{23} denotes the maximum reaction force at 23°C and R_{60} denotes a maximum reaction force at 60°C).

Claim 8 (Cancelled)

9. (Currently Amended) The fender according to ~~claim 8,~~ <u>claim 1</u> wherein the ~~synthetic~~ <u>base</u> rubber is butadiene rubber or styrene-butadiene rubber.